## UM0926 User manual

## STEVAL-ILL019V1 offline RGGB LED driver demonstration board with high PF

## Introduction

The STEVAL-ILL019V1 demonstration board was developed to drive high brightness and power RGGB LEDs used in many different lighting applications. Thanks to RGGB LEDs, it is possible to easily modify the color of the light, change the brightness level, implement additional lighting features such as automatic color changes or a blinking mode, improve lighting efficiency compared to standard lighting products and finally also achieve significant energy savings. Typically, RGGB LED applications can be found as decorative lighting in houses or hotels, as architectural lighting in stadiums, historic buildings, bridges and monuments, as wall washing, shop lighting and in many other special lighting applications.

The STEVAL-ILL019V1 implements an innovative solution for driving multiple color RGGB LEDs, where high Power Factor, safety isolation and individual regulation of LED brightness are required. A constant current is set to 350 mA . Thanks to the microcontroller onboard, the output channels are independently controlled by four PWM signals, allowing the application users to set any color of the light or create automatic color effects. The demonstration board is shown in Figure 1 and its ordering code is STEVAL-ILL019V1.

## STEVAL-ILL019V1 main features

■ Constant LED current: 350 mA

- 4 channels for RGGB LEDs designed on the board

■ Line input voltage range: 88 V to 265 V AC

- Load: 5 to 13 LEDs per each channel
- 32 W maximum RGGB LED power (wide input voltage range)

■ 42 W maximum RGGB LED power (EU input voltage range)
■ Isolated SMPS
■ Individual regulation of RGGB brightness

- EN55015 and EN61000-3-2 compliant

■ Double-sided PCB, $145 \mathrm{~mm} \times 75 \mathrm{~mm} \times 27 \mathrm{~mm}$
Figure 1. STEVAL-ILL019V1 demonstration board

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## 1 Getting started with the STEVAL-ILL019V1

This section allows designers to quickly evaluate the board as the load and external potentiometer connections (to manually control the color of the light) are described.
As already stated, the light color can be changed automatically or manually. The application is set by default to automatic mode in case no potentiometer nor jumper is connected to the board via the J3 connector (see Figure 1). In order to control each LED channel manually, the potentiometers and jumper must be connected to the J3 connector. These two modes are demonstrated in the following sections.

### 1.1 Automatic color change mode

First, the RGGB LEDs must be connected to the board via the output connector J6 (see Figure 1). Four independent channels marked as $\mathrm{CH} 1, \mathrm{CH} 2, \mathrm{CH} 3$ and CH 4 allow controlling four independent LED strings. The LED anode must be connected to the plus (+) pin and the LED cathode must be connected to the minus $(-)$ pin, which is marked close to the connector J6. The recommended minimum LED voltage for each channel is 15 V and the maximum voltage is 40 V , in order to keep the LED current within $\pm 5 \%$. As the typical LED forward voltage is 3.5 V , an LED string with 5 to 11 LEDs per channel must be used. The designers must also take into account that the maximum output LED power is 32 W for wide input voltage range ( 88 V to 265 V AC ) and 42 W for EU input voltage range ( 188 V to 265 V AC ). It is also possible to use only one, two or three channels. A typical example of how the load with RGGB LEDs can be designed is shown in Figure 2 which is also the default RGGB LED load used for measurements on the STEVAL-ILL019V1demonstration board. In this case channel 1 has 6 green LEDs, channel 2 has 8 red LEDs, channel 3 has 7 green LEDs and channel 4 has 9 blue LEDs. This RGGB LED load is just for demonstration purposes and is not available for ordering.

Figure 2. Default RGGB LED load used for testing


The last step after the RGGB LED load connection is to supply the demonstration board with the proper input voltage. The output light color is automatically changed as soon as the input voltage is applied to the board via connector J1.

### 1.2 Manual color change mode

First connect the RGGB LED load to the STEVAL-ILL019V1 as described in the previous section. Then connect the potentiometers to the J3 connector as demonstrated in Figure 3. The control connector has three main purposes. Firstly, it is used in manufacturing to connect the programming station and program the ST7 microcontroller. Secondly, it connects up to four potentiometers to set the brightness of each LED string. For the RGGB LED module, only three potentiometers are used because two green LED strings are driven with the same brightness. The last feature on the connector is a "Mode selection Pin 9" which is used to choose either automatic or manual mode. During automatic mode, pin 9 is internally grounded. A positive voltage of 5 V must be connected to pin 9 (for example to use the switch S) for the manual mode. The automatic mode does not require any action from the user and changes the colors through the color spectrum. The manual mode keeps the color stable based on the position of the potentiometers. The last step is to resupply the board with the proper input voltage. The output light color can be manually tuned as demonstrated in Figure 4. The external control circuitry is again used just for demonstration purposes and is not available for ordering.

Figure 3. J3 connector with manual control circuitry


Figure 4. Different color settings using manual color control


## 2 Design concept

Figure 5 shows the STEVAL-ILL019V1 block diagram. Basically, the board consists of two converters. The first one is in fact an AC/DC converter designed as an isolated high PF flyback converter using the L6562A controller with the STP7NK80ZFP Power MOSFET as a switch. The input voltage for this convertor can be between 88 V and 265 V AC and the converter delivers up to 35 W for this wide input voltage range. The output voltage is set to 48 V . The high Power Factor flyback convertor was already designed separately for demonstration purposes (ordering code is EVL6562A-35WFLB) and therefore all design equations and calculations are described in AN2838 (see Section 7: References).
The second converter is in fact a constant current LED driver. It is a modified buck converter designed as the constant current source recommended for proper LED driving using the L6562A and STS4NF100 Power MOSFETs. Four independent DC/DC converters are assembled on the board in order to drive independent RGGB LED strings. The demonstration board for a modified buck converter was also developed (ordering code is EVL6562A-LED) and this design concept is described in AN2983 (see Section 7: References). All design equations for the modified buck converter are shown in AN2928 (see Section 7: References).

The color control and brightness regulation is provided by the PWM generator which has four independent channels. Each PWM signal is connected to one modified buck converter in order to set the required brightness level for each LED string. The PWM signal can be set between $0 \%$ and $100 \%$ (no brightness or maximum brightness). The ST7FLIT15BF1M6 microcontroller assembled on the board provides the right PWM signals. Thanks to the microcontroller, it is also possible to modify the light effects. The RGGB LED brightness can be set manually, if the external potentiometers are connected to the board via the connector J3.

Figure 5. STEVAL-ILL019V1 block diagram


## 3 STEVAL-ILL019V1 measurements

The most important parameters such as electrical behavior, thermal behavior, dimming function, board power capability and standards (EN55015 and EN61000-3-2) were measured on the STEVAL-ILL019V1demonstration board shown in Figure 6 and the results are given in the following section.

Figure 6. STEVAL-ILL019V1 demonstration board used for measurements


### 3.1 PF, THD efficiency

The power factor (PF) is shown in Figure 7 and Figure 8. Two RGGB LED loads are used for this measurement. Firstly, the default load of 30 W RGGB LEDs ( 9 blue LEDs, 13 green LEDs and 8 red LEDs) was used for the measurement and this load is shown in Figure 2. The second load used for the measurement is 20 W RGGB LEDs ( 5 blue LEDs, 8 green LEDs and 7 red LEDs). The power factor is 0.995 for the input voltage 110 V AC and 0.94 for the input voltage 230 V AC (measured for 30 W load).

The total harmonic distortion (THD) measurement is demonstrated in Figure 9. THD is 8.5 for the input voltage 110 VAC and 14.1 for the input voltage 230 V AC (measured for 30 W load).
The efficiency measurement for these two loads is shown in Figure 10. The efficiency is approximately $75 \%$ for a 30 W load, which is in line with the estimation performance because there are two converters (AC/DC and DC/DC) used in the design.

Figure 7. Power Factor measurement


Figure 8. Power Factor-zoom measurement


Figure 9. Total Harmonic Distortion (THD) measurement


Figure 10. Efficiency measurement


### 3.2 Output current for different number of LEDs

Thanks to the modified buck converter designed as the current source (additional feedback resistors R56, R57, R58 and R59 in the design), it is possible to drive a variable number of LEDs. The output constant current was checked for different numbers of LEDs connected to the modified buck converter and the result is demonstrated in Table 1 and Figure 11. It is recommended to have the output voltage between 15 V and 38 V in order to keep the output LED current within approximately $\pm 5 \%$. An established number of LEDs follows the output voltage recommendation and can be easily calculated as the LED forward voltage is a typical parameter written in any LED datasheet.

Table 1. LED current vs. number of LEDs

| Number of <br> LEDs | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ | $\mathbf{1 0}$ | $\mathbf{1 1}$ | $\mathbf{1 2}$ | $\mathbf{1 3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\mathrm{LED}}[\mathrm{mA}]$ | 390 | 362 | 351 | 346 | 346 | 348 | 350 | 351 | 355 | 357 |
| $\mathrm{~V}_{\mathrm{LED}}[\mathrm{V}]$ | 12.1 | 15 | 17.9 | 20.8 | 23.7 | 26.7 | 29.7 | 32.7 | 35.6 | 38.7 |

Figure 11. Modified buck converter output current


### 3.3 Maximum load capability

One of the most important features regarding this reference design is its maximum power capability because it limits the maximum number of LEDs connected to this board. The power capability measurement for wide input voltage range is shown in Figure 12. The worst case for the measurement is the minimum input voltage and therefore the board was tested with the input voltage 88 V AC. The maximum power is limited by the high PF flyback converter and so its power capability is measured separately (resistive load is connected to the output of the high PF flyback converter - capacitor C10). Figure 12 shows that the output voltage starts to decrease as soon as the load current reaches 0.7 A (blue waveform). As indicated by the red waveform, the maximum output power is limited to 35 W . The inverted buck converters are used as the second stage DC/DC converter and it is possible to estimate their efficiency at $90 \%$ (also measured). Therefore maximum power capability of the STEVAL-ILL019V1 for wide input voltage range is 32 W . Also, the Power MOSFET and transformer temperature was checked after one hour with maximum load ( 35.8 W ) with 88 V input voltage (ambient temperature $25^{\circ} \mathrm{C}$ ). The Power MOSFET had a temperature of $61^{\circ} \mathrm{C}$ and the transformer had a temperature of $60^{\circ} \mathrm{C}$.

The maximum power capability for the EU voltage range ( 188 V to 265 V AC) is also measured, refer to Figure 13. The high PF flyback converter is again measured separately using a resistive load connected to the capacitor C10. In this case the maximum power limit is above 35 W , as the minimum input voltage was set to 188 V AC. Finally, a higher input voltage ( 188 V ) compared to a wide input voltage range ( 88 V ) means that the primary current is lower (avoiding transformer saturation) and therefore the high PF converter is able to deliver higher power to the load for the EU input voltage range. In this case, the maximum
power capability is limited by the temperature of the power components (mainly the transformer and Power MOSFET). The maximum Power MOSFET and inductor temperature was selected at $61^{\circ} \mathrm{C}$ in order to have the same maximum temperature on the transformer and Power MOSFET as that of the wide input voltage range. The temperature was measured after 1 hour and the Power MOSFET had a temperature of $59{ }^{\circ} \mathrm{C}$ and the transformer had a temperature of $61^{\circ} \mathrm{C}$ for load power of 46 W . Efficiency for the inverted buck converter can be again estimated at $90 \%$ and therefore maximum power capability of the STEVAL-ILL019V1 for the EU input voltage range is 42 W as shown in Figure 13.

Figure 12. High PF flyback converter power capability for $\mathrm{V}_{\mathrm{IN}}=88 \mathrm{~V}$ AC


Figure 13. High PF flyback converter power capability for $\mathrm{V}_{\mathrm{IN}}=185 \mathrm{~V}$ AC


### 3.4 Dimming

The dimming function on the STEVAL-ILL019V1 was evaluated. One output channel (channel 4 with 9 blue LEDs) of the inverted buck converter was measured. Figure 14 to Figure 17 show the output LED current and voltage for brightness levels set to 50\%, 10\% and $1 \%$. Thanks to the inverted buck topology, the application can be also completely switched off (no current flows to the LEDs), because the Power MOSFET is turned off by the PWM signal (the L6562A controls the Power MOSFET).

Figure 14. PWM dimming 50\%


Figure 15. PWM dimming $10 \%$


Figure 16. PWM dimming 1\%


Figure 17. PWM dimming 1\%-zoom

### 3.5 Input and output electrical waveforms

The LED current measured for one channel (channel 4 with 9 blue LEDs) is shown in Figure 18. The LED average current is 350 mA , the inverted buck converter switching frequency is 189 kHz and the peak-to-peak LED current ripple is 57.8 mA .

Figure 19 shows the input current and voltage waveforms for the input voltage 110 V AC. The default load of 30 W RGGB LEDs is used for this measurement. In this case the STEVAL-ILL019V1 has PF $=0.995$ and THD $=8.5 \%$.

Figure 20 shows the input current and voltage waveforms for the input voltage 230 V AC. The default load of 30 W RGGB LEDs is again used for this measurement. In this case the STEVAL-ILL019V1 has PF $=0.94$ and $T H D=14.1 \%$.

Figure 18. LED current measurement


Figure 19. Input voltage and current waveforms for $\mathrm{V}_{\text {IN }}=110 \mathrm{~V}$ AC

Figure 20. Input voltage and current waveforms for $\mathrm{V}_{\text {IN }}=230 \mathrm{~V}$ AC


### 3.6 Thermal measurement

Thanks to the thermal chamber and camera, the overall temperature for all the components assembled on the STEVAL-ILL019V1 is easily detected. Figure 21 shows the thermal behavior for ambient temperature $25^{\circ} \mathrm{C}$, input voltage 230 V AC and 30 W RGGB LED load. The maximum temperature is $76.1^{\circ} \mathrm{C}$ and it is measured on the sense resistors R35, R36, R41 and R42, on the Power MOSFET T3 and T4 and also on the linear voltage regulator IC3.

Figure 21. Thermal measurement on the STEVAL-ILL019V1


### 3.7 Standard EN61000-3-2 measurement

If the input power for a lighting application is above 25 W , then it is required to have an active Power Factor Correction (PFC) circuit in the final application. The high PF flyback converter with the L6562A controller (transition mode PFC controller) is perfectly suitable for such applications. Thanks to this design approach, input voltage 110 V AC or input voltage 230 V AC meets the standard EN61000-3-2 as seen in Figure 22 and Figure 23.

Figure 22. EN61000-3-2 compliance for inpu voltage 110 V AC


Figure 23. EN61000-3-2 compliance for input voltage 230 V AC


### 3.8 EMI measurement (EN55015)

The norm EN55015 (CISPR15) describes the limits and methods of measuring radio disturbance characteristics of electrical lighting and similar equipment. The limits of the mains terminal disturbance voltages for quasi-peak measurement for frequency range from 9 KHz to 30 MHz and the real measurement is demonstrated in Figure 24. The test was performed with input voltage $\mathrm{V}_{\mathrm{IN}}=230 \mathrm{~V}$ AC, 30 W RGGB LED load and the LED brightness was set to maximum level. The limits of the mains terminal disturbance voltages for average measurement for frequency range from 150 KHz to 30 MHz and the real measurement is shown in Figure 25. These results comply with the standard EN55015 as shown in Figure 24 and Figure 25.

Figure 24. Quasi-peak measurement from 9 KHz to 30 MHz


Figure 25. Average measurement from 150 KHz to 30 MHz

## 4 Power transformer specifications

Transformer type:

- Winding type: layer
- Core type: ER30
- Coil former: horizontal type, $9+9$ pins (see dimensions in Figure 26)
- Mains insulation: 4 KV

Figure 26. Transformer frame dimensions


Electrical specifications for the transformer:

- Converter topology: flyback, TM mode
- Ferrite material PC40 or similar for SMPS
- Min. operating frequency: 36 kHz
- Inductance factor approximately $\mathrm{AI}=90 \mathrm{nH}$; air gap in central leg
- Primary inductance 1.61 mH
- Primary winding N1 + N2 = 134 turns

Table 2. Transformer design specifications

| Winding | Layer <br> sequence | Start pin <br> number | Finish pin <br> number | Turns | Wire diameter <br> $(\mathbf{m m})$ | Side |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N1 | 5 | 3 | 1 | 67 | 0.4 | Primary |
| N2 | 2 | 5 | 3 | 67 | 0.4 | Primary |
| N3 | 1 | 8 | 7 | 13 | 0.2 | Primary |
| N4 | 3 | $17,(18)$ | $14,(15)$ | 33 | $2^{\star 0.4}$ | Secondary |
| N5 | 4 | 11 | 12 | 17 | 0.2 | Secondary |
| N6 | $9-$ over core | 8 | 8 | 1 | Cu foil | Shielding |

Note: $\quad$ Intersperse winding N3, N5 through as much of the winding area as possible in order to reduce the leakage inductance (since these windings do not completely fill a layer, the winding should be spaced evenly across the layers).
Each layer of windings N1 and N2 must be isolated by a single layer of Mylar ${ }^{\circledR}$ Tape.
Figure 27. Transformer winding description


Figure 28. Winding position on the transformer


## 5 Schematic diagrams

Figure 29. High PF flyback converter


Figure 30. Four modified buck converters and microcontroller


## 6 Bill of material

Table 3. Bill of material - STEVAL-ILL019V1

| I | Q | Reference | Part | Type | Manufacturer | Ordering code |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | C1 | $220 \mathrm{nF} / \sim 305 \mathrm{~V}$ AC | X2 capacitor | EPCOS | B32923C3224M |
| 2 | 1 | C2 | $150 \mathrm{nF} / \sim 305 \mathrm{~V}$ AC | X2 capacitor | EPCOS | B32922C3154M |
| 3 | 1 | C3 | 470 nF / ~305 V AC | X2 capacitor | EPCOS | B32923C3474M |
| 4 | 1 | C4 | $2.2 \mathrm{nF} / 63 \mathrm{~V}$ | 0805 SMD capacitor |  |  |
| 5 | 1 | C5 | $220 \mathrm{nF} / 63 \mathrm{~V}$ | 0805 SMD capacitor |  |  |
| 6 | 23 | C6, C12, C13, C14, C15, C19, C20, C23, C24, C25, C28, C29, C30,C33, C34, C35, C38, C39, C40, C41, C42, C43, C45 | $100 \mathrm{nF} / 63 \mathrm{~V}$ | 0805 SMD capacitor |  |  |
| 7 | 2 | C7, C11 | 47 ¢F / 35 V | Electrolytic capacitor |  |  |
| 8 | 1 | C8 | $330 \mathrm{pF} / 63 \mathrm{~V}$ | 0805 SMD capacitor |  |  |
| 9 | 2 | C9, C10 | $1 \mathrm{mF} / 63 \mathrm{~V}$ | Electrolytic capacitor | EPCOS | B41821F8108M |
| 10 | 1 | C16 | 2.2 F / 25 V | 1206 ceramic capacitor X7R | AVX | 12063C225KAT2A |
| 11 | 1 | C17 | $4.7 \mu \mathrm{~F} / 63 \mathrm{~V}$ | Electrolytic capacitor |  |  |
| 12 | 1 | C18 | $1 \mathrm{nF} / 250 \mathrm{~V}$ AC | Y1 capacitor | Murata Manufacturing Co., Ltd. | DE1E3KX102MA5B |
| 13 | 8 | $\begin{aligned} & \mathrm{C} 21, \mathrm{C} 22, \mathrm{C} 26, \\ & \mathrm{C} 27, \mathrm{C} 31, \mathrm{C} 32, \\ & \mathrm{C} 36, \mathrm{C} 37 \end{aligned}$ | $330 \mathrm{pF} / 63 \mathrm{~V}$ | 0805 SMD capacitor |  |  |
| 14 | 1 | C44 | $10 \mathrm{nF} / 63 \mathrm{~V}$ | 0805 SMD capacitor |  |  |
| 15 | 1 | DB1 | $1 \mathrm{~A} / 250 \mathrm{~V}$ | Diode bridge SMD |  |  |
| 16 | 1 | D1 | P6KE300A | Transil ${ }^{\text {TM }}$ unidirectional 300 V | STMicroelectronics | P6KE300A |
| 17 | 1 | D2 | STTH1R06U | 1 A / 600 V ultrafast diode | STMicroelectronics | STTH1R06U |
| 18 | 15 | $\begin{aligned} & \text { D3, D7, D8, D9, } \\ & \text { D11, D13, D15, } \\ & \text { D17, 18, D19, } \\ & \text { D20, D22, D23, } \\ & \text { D24, D25 } \end{aligned}$ | 1N4148 | 150 mA / 75 V universal diode |  |  |
| 19 | 1 | D4 | STTH3R02S | 3 A / 200 V ultrafast diode | STMicroelectronics | STTH3R02S |
| 20 | 1 | D5 | STTH102A | 1 A / 200 V ultrafast diode | STMicroelectronics | STTH102A |

Table 3. Bill of material - STEVAL-ILL019V1 (continued)

| I | Q | Reference | Part | Type | Manufacturer | Ordering code |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 21 | 1 | D6 | BZV55C15 | 15 V Zener diode (SOD80) |  |  |
| 22 | 4 | $\begin{aligned} & \text { D10, D12, D14, } \\ & \text { D16 } \end{aligned}$ | STPS1H100A | 1 A / 100 V Schottky diode | STMicroelectronics | STPS1H100A |
| 23 | 1 | D21 | BZV55C30 | 30 V Zener diode (SOD80) |  |  |
| 24 | 1 | F1 | 2.5 A / 250 V | Fuse |  |  |
| 25 | 1 | F1 | Fuse socket |  |  |  |
| 26 | 5 | H1, H2, H3, H4, T1HEAT | Screw | Screw $3 \times 6 \mathrm{~mm}$ |  |  |
| 27 | 4 | H11, H22, H33, H44 | Column distance | 15 mm |  |  |
| 28 | 5 | $\begin{aligned} & \text { IC1, IC5, IC6, } \\ & \text { IC7, IC8 } \end{aligned}$ | L6562AD | PFC controller | STMicroelectronics | L6562AD |
| 29 | 1 | IC2 | TL431AID | Programmable voltage reference | STMicroelectronics | TL431AID |
| 30 | 1 | IC3 | L78M15ACDT | Linear voltage regulator | STMicroelectronics | L78M15ACDT |
| 31 | 1 | IC4 | L78L05ACD13TR | Linear voltage regulator | STMicroelectronics | L78L05ACD13TR |
| 32 | 1 | IC9 | ST7FLIT15BF1M6 | Microcontroller | STMicroelectronics | ST7FLIT15BF1M6 |
| 33 | 1 | J1 | ARK120/2 | Input connector |  |  |
| 34 | 2 | J3, J6 | S1G40 | Control connector 40-pin |  |  |
| 35 | 1 | L1 | B82732F2451B001 | Frame core chokes $2 \times 100 \mathrm{mH} / 0.45 \mathrm{~A}$ | EPCOS | B82732F2451B001 |
| 36 | 4 | L2, L3, L4, L5 | MSS1260-105KLD | $1 \mathrm{mH} / 0.4 \mathrm{~A}$ | Coilcraft | MSS1260-105KLD |
| 37 | 1 | Ol1 | PC817B | Optocoupler |  |  |
| 38 | 2 | R1, R2 | $1.5 \mathrm{M} \Omega$ | 1206 SMD resistor |  |  |
| 39 | 2 | R3, R6 | $22 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 40 | 1 | R4 | $9.1 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 41 | 2 | R5, R22 | $39 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 42 | 3 | R7, R20, R21 | $2.2 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 43 | 2 | R8, R9 | $220 \mathrm{~K} \Omega$ | 1206 SMD resistor |  |  |
| 44 | 6 | $\begin{aligned} & \text { R10, R13, R27, } \\ & \text { R33, R39, R45 } \end{aligned}$ | $10 \Omega$ | 0805 SMD resistor |  |  |
| 45 | 2 | R11, R23 | $47 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 46 | 6 | R12, R18, R28, R34, R40, R46 | $1 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |

Table 3. Bill of material - STEVAL-ILL019V1 (continued)

| I | Q | Reference | Part | Type | Manufacturer | Ordering code |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | 2 | R14, R15 | $1.3 \Omega$ | 1206 SMD resistor |  |  |
| 48 | 1 | R16 | $1.5 \Omega$ | 1206 SMD resistor |  |  |
| 49 | 3 | R17, R19, R54 | $4.7 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 50 | 1 | R24 | $3.9 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 51 | 4 | $\begin{aligned} & \text { R25, R31, R37, } \\ & \text { R43 } \end{aligned}$ | $2.7 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 52 | 4 | $\begin{aligned} & \text { R26, R32, R38, } \\ & \text { R44 } \end{aligned}$ | $1.5 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 53 | 8 | $\begin{aligned} & \text { R29, R30, R35, } \\ & \text { R36, R41, R42, } \\ & \text { R47, R48 } \end{aligned}$ | $5.6 \Omega$ | 1206 SMD resistor |  |  |
| 54 | 4 | $\begin{aligned} & \text { R49, R50, R51, } \\ & \text { R52 } \end{aligned}$ | $1.8 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 55 | 1 | R53 | $390 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 56 | 1 | R55 | $10 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 57 | 4 | R56, R57, R58, R59 | $160 \mathrm{~K} \Omega$ | 0805 SMD resistor |  |  |
| 58 | 1 | TR1 | ER30 core | Specified in this document | TDK |  |
| 59 | 1 | T1 | STP7NK80ZFP | Power MOSFET 9 A / 800 V | STMicroelectronics | STP7NK80ZFP |
| 60 | 1 | T1HEAT | HEATSINK |  |  |  |
| 61 | 4 | T2, T3, T4, T5 | STS4NF100 | Power MOSFET <br> 4 A / 100 V | STMicroelectronics | STS4NF100 |

## 7 References

1. STMicroelectronics, Application note AN2838, 35 W wide-range high power factor flyback converter demonstration board using the L6562A; see www.st.com.
2. STMicroelectronics, Application note AN2983, Constant current inverse buck LED driver using L6562A, see www.st.com.
3. STMicroelectronics, Application note AN2928, Modified buck converter for LED applications, see www.st.com.

## 8 Revision history

Table 4. Document revision history

| Date | Revision | Changes |
| :---: | :---: | :--- |
| 25-Oct-2010 | 1 | Initial release. |

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